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⑮ Two-solution acrylic adhesive composition.

⑮ A two-solution acrylic adhesive composition, consisting of a solution A, in which the following ingredients (1)-(3) are dissolved and mixed as necessary ingredients, in the proportions mentioned below, and a solution B, in which the following ingredients (4)-(6) are dissolved and mixed as necessary ingredients, in the proportions mentioned below:

Solution A: (1) 12,5-35 wt% chlorosulfonated polyethylene, (2) 50-85 wt% of at least one (meth)-acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)-acrylates with hydroxyl, glycidyl, or amino groups and (3) 0,2-10 wt% of a organic peroxide;

Solution B: (4) 10-25 wt% butadiene-acrylonitrile copolymer elastomer, (5) 40-90 wt% of at least one (meth)acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)acrylates with hydroxyl, glycidyl, or amino groups, and (6) 1-20 wt% of a curing accelerator consisting of an amine-aldehyde condensate. This adhesive composition has excellent resistance to thermal deterioration and excellent workability.

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Two-solution acrylic adhesive composition

Two-solution acrylic adhesives, characterized by the facts that they contain various elastomer ingredients dissolved in reactive acrylic monomers and are cured with redox catalysts, have been widely used for some time. Examples of such two-solution acrylic adhesives are those shown in Public Patent Disclosure Bulletins Nos. 49-132119, 51-7040, and 55-129470. As can be seen in these examples, the general method 5 of sticking two objects together is that a (meth)acrylate solution containing a chlorosulfonated polyethylene and a polymerization initiator (main adhesive) is applied to one of the objects and a curing accelerator such as an amine-aldehyde condensate is applied to the other one; the two surfaces to which these solutions have been applied are then put into contact with each other. In this type of adhesive, since the acrylic monomer is graft-polymerized onto the chlorosulfonated polyethylene in the curing process, the advantages 10 are obtained that the shrinkage rate is comparatively small, and there is excellent heat resistance. On the other hand, however, since a large quantity of chlorine is present in the chlorosulfonated polyethylene structure, there is the problem that when the adhesive is used on metal surfaces, and the parts to which the adhesive was applied are left under a high temperature for a long period, the aforementioned chlorine is eliminated and corrodes the metal surfaces. Moreover, there is the problem that, since the viscosities of 15 curing accelerators containing amine-aldehyde condensates, etc., are low, the curing accelerator penetrates into the surface to which the adhesive is applied when the objects to which the adhesive is to be applied have porous surfaces, such as wood or foams, and after they are adhered together the adhesive strength is uneven; moreover, since the quantity of curing accelerator used is very small, it is difficult to control the correct quantity that must be applied.

20 Therefore, it has been proposed that the curing accelerator solution be thickened with an acrylic rubber or acrylic resin (Public Patent Disclosure Bulletin No. 61-51072), or an epichlorohydrin rubber (Public Patent Disclosure Bulletin No. 56-74165).

However, the aforementioned acrylic rubbers have poor solubilities in (meth)acrylate monomers, and if 25 the quantity compounded is increased, a gel is formed and uniform mixing is prevented. Moreover, the strength of the adhered layers after the two solutions are mixed and cured is still insufficient.

Acrylic resins have good solubilities in (meth)acrylate monomers, but it is necessary to compound a large quantity of such resins in order to obtain the target viscosity, and the rubber elasticity of the adhered layers which is obtained when a large quantity of the resin is compounded is lost, which is not desirable. Moreover, the spinnability of these resins is strong, which presents a problem of workability.

30 In addition, epichlorohydrin rubber, in addition to having the same problems as the aforementioned acrylic rubber, has a large quantity of chlorine in its molecule, like the chlorosulfonated polyethylene, and when it is exposed to high temperatures for long periods, the free chlorine corrodes the adhesion interface.

This invention was made with this situation in view, and has the purpose of providing a two-solution acrylic adhesive composition with excellent resistance to thermal deterioration and excellent workability.

35 In order to accomplish this purpose, the two-solution acrylic adhesive composition of this invention consists of a solution A, in which the following ingredients (1)-(3) are dissolved and mixed as necessary ingredients, in the proportions mentioned below, and a solution B, in which the following ingredients (4)-(6) are dissolved and mixed as necessary ingredients, in the proportions mentioned below:

40 Solution A		
(1) Chlorosulfonated polyethylene	12.5-35 wt %	
(2) At least one (meth)acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)acrylates with hydroxyl, glycidyl, or amino groups	50-85 wt %	
(3) Organic peroxide	0.2-10 wt %	

Solution B		
	(4) Butadiene-acrylonitrile copolymer elastomer	10-25 wt %
5	(5) At least one (meth)acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)acrylates with hydroxyl, glycidyl, or amino groups	40-90 wt %
10	(6) Curing accelerator consisting of an amine-aldehyde condensate	1-20 wt %

The inventors performed a series of studies with the purpose of improving the workability and thermal deterioration resistance of two-solution acrylic adhesive compositions containing chlorosulfonated polyethylenes in the main adhesive; as a result, they discovered that if butadiene-acrylonitrile copolymer elastomers (NBR) are used to regulate the viscosity of solution B, and the proportions of the various necessary ingredients of solutions A and B are limited as mentioned above, the desired purposes can be accomplished, and thus they achieved this invention. They also discovered that if specific styrene block copolymers are included in at least one of the aforementioned solutions A and B, the spinnability during application, which was a problem previously, is improved, in addition to the aforementioned effects.

20 Next, this invention will be explained in detail.

The two-solution acrylic adhesive composition of this invention is composed of a solution A which has as its necessary ingredients (1) a chlorosulfonated polyethylene, (2) a (meth)acrylate monomer, and (3) an organic peroxide, and a solution B which has as its necessary ingredients (4) an NBR, (5) a (meth)acrylate monomer, and (6) an amine-aldehyde condensate.

25 As the chlorosulfonated polyethylene (1), which is a necessary ingredient of the aforementioned solution A, one can use any one, but those with chlorine contents of 20-45% and Mooney viscosities (ML 1+4, 100 °C) of about 20-100 are especially suitable. As commercial products of this kind, *Haiparon* (made by Dupont Co.), etc. are known. Moreover, the content of the chlorosulfonated polyethylene in solution A must be 12.5-35 wt %) (abbreviated below as "%"); a range of 20-30% is especially suitable. If the quantity of 30 chlorosulfonated polyethylene is less than 12.5%, it is difficult to obtain a practical adhesive strength, and if it is greater than 35%, the viscosity of solution A becomes too high, and its miscibility with solution B becomes poor.

35 As the (meth)acrylate monomer (2) which is also a necessary ingredient of solution A, one can use any of the following: (meth)acrylic acid, ethyl (meth)acrylate, propyl (meth)acrylate, butyl (meth)acrylate, isobutyl (meth)acrylate, 2-ethylhexyl (meth)acrylate, isodecyl (meth)acrylate, lauryl (meth)acrylate, stearyl (meth)acrylate, alkyl (meth)acrylates of C₁₀-C₁₈, cyclohexyl (meth)acrylate, isobornyl (meth)acrylate, 2-hydroxyethyl (meth)acrylate, 2-hydroxypropyl (meth)acrylate, dimethylaminoethyl (meth)acrylate, dimethylaminoethyl (meth)acrylate, diethylaminoethyl (meth)acrylate, diethylaminoethyl (meth)acrylate, ethylene glycol dimethacrylate, diethylene glycol dimethacrylate, tetraethylene glycol dimethacrylate, trimethylol propane trimethacrylate, 1,6-hexanediol dimethacrylate, 2-methacryloyloxyethyl succinate, 2-methacryloyloxyethyl phthalate, glycidyl methacrylate, dimethylaminomethyl methacrylate, mono(2-methacryloyloxyethyl)acid phosphate, mono(2-acryloyloxyethyl)acid phosphate, tetrahydrofurfuryl methacrylate, *n*-butoxyethyl methacrylate, methylfulbitol methacrylate and methylsorbitol methacrylate, methyltriglycol methacrylate, butanediol dimethacrylate, neopentylglycol dimethacrylate, epoxy (meth)acrylates which are adducts of epoxy compounds and (meth)acrylic acid, urethane poly(meth)acrylates, cyanoacrylates, etc. These compounds may be used individually or in combinations of two or more. The content of the (meth)acrylate monomer must be in the range of 50-85%. If the (meth)acrylate monomer content is less than 50%, the viscosity of the solution will become too high, and the application workability will be poor; if, on the contrary, it is greater than 85%, the viscosity will become too low and the application workability will also be poor, as well as the proportion of the rubber ingredient becoming too low, so that a cured product with rubber elasticity is not obtained.

55 Other monomers besides the aforementioned (meth)acrylate monomers, such as styrene, acrylonitrile, vinyl acetate, vinyl versatate, or other vinyl ester monomers can be added in suitable quantities, depending on the kind of objects to which the adhesive is to be applied. However, the quantity of such monomers added is limited to 20% or less of solution A. That is, if it is greater than 20%, the adhesive properties of the adhesive will be limited, and it will not be able to be widely used, or a separation phenomenon will be produced in solution A during storage in the tube.

As the organic peroxide (3) which is also a necessary ingredient of solution A, one can use tertiary butyl peroxide, cumene hydroperoxide, diisopropylbenzene hydroperoxide, di-tertiary-butyl peroxide, tertiary butyl

cumyl peroxide, dicumyl peroxide, methylethylketone peroxide, benzoyl peroxide, etc. These compounds can be used individually or in combinations of two or more. These organic peroxides must be contained in solution A in a range of 0.2-10%; a range of 0.5-5% is especially suitable.

On the other hand, the NBR (4) which is a necessary ingredient of solution B is selected especially for this invention, so that its miscibility with the (meth)acrylate solution of chlorosulfonated polyethylene is good, and it does not markedly change the properties of the adhesive, such as adhesive strength, adhesive heat resistance, and curing rate, even when it is used together with the chlorosulfonated polyethylene in large quantities. The nitrile content of such NBR should be 18-45%. Moreover, NBR containing carboxyl, amino, and vinyl groups in their molecules may also be used. Furthermore, if a hydrogenated NBR is used, an adhesive with still greater resistance to thermal deterioration will be obtained. The content of the aforementioned NBR in solution B must be 10-25%; a range of 12.5-20% is still more desirable. If it is less than 10%, the viscosity of solution B will be reduced, and if it is greater than 25%, the viscosity of solution B will be increased; in either case, the workability will be poor.

The (meth)acrylate monomer (5) which is a necessary ingredient of solution B may be any of the (meth)acrylate monomers (2) in solution A mentioned above. Its content must be in the range of 40-90%.

As the curing accelerator (6) composed of an amine-aldehyde condensate which is a necessary ingredient of solution B, one can use, for example, a condensate of a butyl aldehyde and an aniline or butylamine; ordinarily, one uses the commercial products Accelerator 808, Accelerator 833 (both made by E. I. Dupont de Nemours Co.), Nokusera 8 (Ouchi Shinko Kagaku Kogyo Co.), etc. The content of the aforementioned curing accelerator must be 1-80% of solution B; a range of 2-15% is especially desirable. If the aforementioned curing accelerator is less than 1%, the curing when the two solutions are mixed will be slow, and sufficient adhesive strength cannot be obtained. Conversely, if it is greater than 20%, the excess portion of the curing accelerator acts as a plasticizer, and the adhesive strength is reduced. Moreover, since the viscosity of the whole solution B is reduced, its uniform miscibility with solution A becomes worse.

Furthermore, in this invention, when solutions A and B are prepared by using the aforementioned necessary ingredients, it is desirable to make the monomer ingredients of solutions A and B as close to each other as possible. For the degree of closeness of the aforementioned monomer ingredients, the difference in the secondary transition temperatures T_g of the monomer copolymers of the two solutions can be used as a criterion; it has been found that this difference should be within 80 °C, especially 65 °C. The secondary transition temperature of the aforementioned monomer copolymers can be easily obtained from the following formula of Fox:

$$\frac{1}{T_g} = \frac{w_1}{T_{g1}} + \frac{w_2}{T_{g2}} + \dots \dots \dots + \frac{w_n}{T_{gn}}$$

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(where w_1, w_2, \dots, w_n are the weight fractions of each monomer and $T_{g1}, T_{g2}, \dots, T_{gn}$ are the secondary transition temperatures of the various monomer single polymers).

Moreover, the viscosities of the two solutions should be made close to each other by having solution A as well as solution B contain the elastomer NBR. That is, by having solution A contain NBR in the range of 15% or less, so that the ratio of the elastomer ingredient content W_a of solution A and the elastomer ingredient content W_b of solution B (W_a/W_b) is made 0.5-3.0 by weight, an adhesive layer with excellent adhesive strength is obtained when a two-solution separate type adhesive is applied. Furthermore, the aforementioned elastomer ingredient is chlorosulfonated polyethylene, NBR, or other elastic substances.

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The two-solution acrylic adhesive composition obtained in this way may be applied by applying solutions A and B separately, and making the two surfaces on which they are applied adhere, as with conventional two-solution acrylic adhesives. It is desirable, however, for the two liquids to be mixed before they are used, insofar as is possible. If this is done, there is no need to consider the balance of the two solutions carefully, and not only will the application workability be good, but an adhesive layer can be formed which will have a high resistance to thermal deterioration, which could not be obtained previously. This appears to be because the NBR used as a necessary ingredient does not have chlorine in its molecular structure.

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Furthermore, the inventors discovered that if a styrene block copolymer is added to either solution A or solution B of the two-solution acrylic adhesive composition of this invention, or both solutions, the spinnability when the adhesive is applied, which was a problem previously, is improved. For the aforementioned styrene block copolymer, one can use, for example, styrene-butadiene-styrene block copolymers, styrene-isoprene-styrene block copolymers, styrene-ethylene-butylene-styrene block copolymers, styrene-

ethylene-propylene-styrene block copolymers, styrene-butadiene block copolymers, styrene-isoprene block copolymers, styrene-ethylene-butylene block copolymers, or styrene-ethylene-propylene block copolymers. Especially desirable ones are styrene-ethylene-butylene-styrene block copolymers and styrene-ethylene-propylene-block copolymers. These may be used individually or in combinations of two or more.

5 Furthermore, commercial products of such styrene block copolymers are *Karifurekkus* and *Kureiton* (both made by Shell Kagaku Co.). The quantity of the aforementioned styrene block copolymer used should be 5-200%, preferably 10-140%, with respect to the elastomer ingredient. If the quantity added is less than 5%, the curing which improves the spinnability will be small, and if it is greater than 200%, the viscosity and thixotropy of the solution to which it is added will become too high.

10 Besides the aforementioned ingredients of the two-solution acrylic adhesive composition of this invention, one can also add, if desired, suitable quantities of coloring agents, paraffin, fillers, anti-oxidants, epoxy resins or other chlorine trappers, cobalt naphthenate, copper naphthenate, magnesium naphthenate, or other metal soaps, or curing accelerators such as dimethyl-*p*-toluidine, diethyl-*p*-toluidine, diethanol-*p*-toluidine, diisopropanol-*p*-toluidine, thiourea, ethylene urea, acetylthiourea, tetramethyl thiourea, dibutyl thiourea, mercaptobenzimidazole, etc.

15 As mentioned above, the two-solution acrylic adhesive composition of this invention has good workability, since it may be used in the two-solution separate form, as with conventional adhesives, or applied after the two solutions are mixed. Furthermore, the adhesive layer obtained has excellent thermal deterioration resistance; even when it is used in adhering metals, corrosion of the adhered surfaces is suppressed, and it is possible to preserve good adhesion over long periods. Consequently, the two-solution acrylic adhesive composition of this invention can be used in a wide range of applications, including not only the adhesion of construction panels, bathroom basins, solar panels, automobile door panels, etc., but also the adhesion of electrical machinery parts requiring heat resistance and thermal deterioration resistance, such as speaker and motor magnets, etc.

20 25 Next, actual examples of this invention will be explained.

First, before the actual examples, 15 solutions A were prepared, as shown in Table 1 below, and 15 solutions B were prepared, as shown in Table 2 below. The viscosities of the solutions were investigated, and their states of composition were observed by the naked eye. These results are shown in Tables 1 and 2.

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Table 1

		A 1	A 2	A 3	A 4	A 5	A 6	A 7	A 8	A 9	A 10	A 11	A 12	A 13	A 14	A 15
a	b	35	30	25	20	12.5	40	10	20	15	20	20	20	20	20	20
N	C	—	—	—	—	—	—	—	—	5	—	—	—	—	—	—
B	C	—	—	—	—	—	—	—	—	—	15	—	—	—	—	—
R	C	—	—	—	—	—	—	—	—	—	—	5	—	—	—	—
d	d	—	—	—	—	—	—	—	—	—	—	—	5	—	—	—
e	e	—	—	—	—	—	—	—	—	—	—	—	—	5	—	—
f	f	—	—	—	—	—	—	—	—	—	—	—	—	—	5	—
g	Gechron CR-2000	—	—	—	—	—	—	—	—	—	—	—	—	—	—	5
h	h	32.5	57.3	62.0	52.5	59.0	38.0	77.0	62.0	37.0	32.5	62.0	62.0	62.0	62.0	62.0
i	i	—	—	—	—	15	—	—	—	—	—	—	—	—	—	—
j	j	10	5	10	—	5	5	10	10	10	—	10	—	10	10	10
k	k	10	5	—	10	5	—	—	—	20	30	—	10	—	—	—
l	l	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
m	m	10	0.2	0.5	5	1	15	0.5	0.5	0.5	10	0.5	0.5	0.5	0.5	0.5
n	n	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
(cps/25°C) o	(cps/25°C) o	40000	15000	4000	2000	500	90000	180	12800	18000	13000	12800	15000	10000	45000	1500
p	p	q	q	q	q	q	q	r	q	q	q	q	q	s	r	q

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- a. Composition
- b. Haiparōn
- c. Nipōru
- 5 d. Zettopōru
- e. Acrylic resin Hararoido A-30
- f. Acrylic rubber Haika 4051 EP
- 10 g. Epichlorohydrin rubber
- h. Methyl methacrylate
- i. Isobutyl methacrylate
- j. Methacrylic acid
- k. Hydroxyethyl methacrylate
- l. Ethylene glycol dimethacrylate
- m. Cumene hydroperoxide
- n. 2,5-di-tertiary-butyl-hydroquinone
- o. Viscosity
- p. Composition stability
- q. Good
- r. Gelled
- s. Separated

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Table 2

		B 1	B 2	B 3	B 4	B 5	B 6	B 7	B 8	B 9	B 10	B 11	B 12	B 13	B 14	B 15
a																
N	b	25	20	17.5	10	10	30	5	17.5	10	—	—	—	—	—	—
B	b	—	—	—	2.5	—	—	—	—	5	15	—	—	—	—	—
R	b	—	—	—	—	—	—	—	—	—	—	10	—	—	—	—
C		—	—	—	—	—	—	—	—	—	—	—	15	—	—	—
d		—	—	—	—	—	—	—	—	—	—	—	—	15	—	—
e		—	—	—	—	—	—	—	—	—	—	—	—	—	10	—
f		—	—	—	—	—	—	—	—	—	—	—	—	—	—	15
Gehron CR-2000		40	50	72.5	83	86.5	52.5	92	55	72.5	45	80	65	75	80	75
g		—	—	—	—	—	—	—	—	—	20	—	—	—	—	—
h		12.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—
i		—	12.5	—	—	—	—	—	—	—	—	—	—	—	—	—
j		—	—	—	—	—	—	—	—	—	10	—	10	—	—	—
k		2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
l		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
m		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05
n		20	15	7.5	2	1	15	0.5	25	10	7.5	7.5	7.5	7.5	7.5	7.5
o		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
(cps/25°C) P		28000	9000	4000	2000	800	710	75	2500	4500	5000	2200	7500	5400	710	13000
r		s	s	s	s	s	s	s	s	t	n	s	s	s	s	s

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- a. Composition
- b. Nipōru
- c. Zettōpōru
- 5 d. Acrylic resin Hararoldo A-30
- e. Acrylic rubber Harka 4051 EP
- f. Epichlorohydrin rubber
- 10 g. Methyl methacrylate
- h. Isobutyl methacrylate
- i. Butyl acrylate
- j. Hydroxyethyl methacrylate
- k. Ethylene glycol dimethacrylate
- 15 l. 2,5-di-tertiary-butyl-hydroquinone
- m. Copper naphthenate
- n. Butylaldehyde-aniline condensate Nokuserā-8
- o. Oil blue
- p. Viscosity
- q. × 10,000
- r. Composition stability
- s. Good
- t. Gelled
- u. Low viscosity
- v. Spinnable

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(Actual Examples 1-10, Comparison Examples 1-5)

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The 15 kinds of solution A shown in Table 1 and the solution B shown as B3 in Table 2 were mixed rapidly in equal quantities by weight, and the workabilities of mixing with solution B and applying were observed, after which [these adhesives] were used to adhere resins to each other and sanded spec [sic] copper plates to each other. Moreover, after leaving [these samples] at room temperature for 1 day, their tensile shear strengths were measured (measurement temperature: 20 °C, pulling speed: 3mm/min).

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Furthermore, these adhered bodies were left for 2 months at 120 °C, after which the temperature was returned to 20 °C and the tensile shear strengths were measured. These results are shown in Table 3 below.

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Table 3

d (kg/dL)	a					b					a					b						
	1	2	3	4	5	1	2	6	7	8	9	10	3	4	5	1	2	6	7	8	9	10
c	○	○	○	○	○	×	×	○	○	○	○	○	○	○	○	○	○	○	○	○	○	
e 1.	235	228	217	210	168	—	135	215	182	211	209	206	228	—	210	—	—	—	—	—	—	—
f	215	216	219	213	177	—	150	221	200	208	210	203	206	—	165	—	—	—	—	—	—	—

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- a. Actual Examples
- b. Comparison Examples
- c. Stability of mixture with B3

- d. Tensile shear strength
- e. After standing for 1 day
- f. After 2 months at 120°C

55 From these results, it can be seen that the actual examples in which solutions A with a chlorosulfonated polyethylene content of 12.5-35% were used, or the actual examples in which some of solution A was

replaced with nitrile rubber, had excellent states of composition, miscibility with solution B and applicability, adhesive strength, and resistance to thermal deterioration.

5 (Actual Examples 11-19, Comparison Examples 6-11)

The 16 kinds of solution B shown in Table 2 and the solution A shown as A3 in Table 1 were mixed rapidly in equal quantities by weight, and the workabilities of mixing with solution A and applying were observed, after which these adhesives were used to adhere resins to each other and sanded spec copper plates to each other. Moreover, after leaving these samples at room temperature for 1 day, their tensile shear strengths were measured (measurement temperature: 20 °C, pulling speed: 3mm/min).

Furthermore, these adhered bodies were left for 2 months at 120 °C, after which the temperature was returned to 20 °C and the tensile shear strengths were measured. These results are shown in Table 4 below.

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Table 4

	a	b															
		11	12	13	14	15	6	7	8	16	17	18	19	9	10	11	
c	○	○	○	○	○	○	×	×	○	○	○	○	○	○	×	○	
d	1 e	180	193	217	225	185	-	87	98	220	181	230	216	240	98	210	
(kg/cm²)	120	12. 2.	f	195	197	219	216	164	-	126	101	229	186	232	217	165	120
																113	

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- a. Actual Examples
- b. Comparison Examples
- c. Stability of mixture with A3

- d. Tensile shear strength
- e. After standing for 1 day
- f. After 2 months at 120°C

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From these results, it can be seen that the actual examples in which solutions B with an NBR content of 10-25% and butaldehyde-aniline condensate contents of 1-20% were used had excellent states of composi-

tion, miscibility with solution A and applicability, adhesive strength, and resistance to thermal deterioration.

(Actual Examples 20-25, Comparison Examples 12, 13)

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Using the combinations of solutions A and B shown in Table 5 below, adhesion of resins to each other and sanded spec copper plates to each other was performed. Moreover, the case in which solutions A and B were used unmixed (solution A applied to one of the objects and solution A and an equal quantity of solution B applied to the other object, after which the surfaces to which they were applied were stuck together) and the case in which they were used after being mixed (equal weights of solutions A and B mixed for 30 seconds, and the whole solution confirmed to have a uniform green color, after which the adhesion was performed rapidly) were used in the measurement of the tensile shear adhesive force. The measurements were performed with a number $n=5$ for adhered objects under the same conditions. These results are shown in Table 5 below.

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Table 5

	a						b
		20	21	22	23	24	
C	A2	A4	A3	A3	A4	A5	A7
d	30	20	25	25	20	125	35
e	B11	B11	B9	B12	B2	B1	B5
f	10	10	15	15	20	25	10
W _a / W _b	3.0	2.0	1.7	1.7	1.0	0.5	3.5
g	173	165	178	177	165	155	154
	205	202	196	200	187	169	219
k	149	169	165	160	151	130	93
	231	236	220	216	198	179	230
	240	241	230	225	205	190	239
	223	229	212	209	190	171	224
							15.9

- a. Actual Examples
- b. Comparison Examples
- c. Kind of solution A
- 5 d. W_a of elastomer in solution A (wt %)
- e. Kind of solution B
- f. W_b of elastomer in solution B (wt %)
- g. Tensile shear strength by non-mixed adhesion
- h. Average value
- i. Maximum value
- j. Minimum value
- 10 k. Tensile shear strength by mixed adhesion

10 From these results, it can be seen that when solutions A and B are used without mixing, those in which the ratio W_a/W_b of the elastomer ingredient contents in solutions A and B is in the range 0.5-3.0 had comparatively small scattering of the adhesive strength, and when solutions A and B were mixed before use, their adhesive strengths are high and the scattering small whatever the ratios of the elastomer compositions of solutions A and B are.

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(Actual Examples 26-38)

20 First, as shown in Table 6 below, solutions A and B were prepared such that the copolymer compositions had (meth)acrylate monomer parts with various glass transition temperatures. The secondary transition temperatures of the various compositions (T_{gA} , T_{gB}) were obtained by calculating according to the method described above. In this calculation, since the quantity of the di-(meth)acrylate monomer used is ordinarily small, it was ignored, and the secondary transition temperatures were obtained by assuming that the other ingredients of solutions A and B have no effects on the glass transition temperatures of the 25 (meth)acrylate monomer copolymers.

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Table 6

		a										b						
		A16	A17	A18	A19	A20	A21	A22	A23	B16	B17	B18	B19	B20	B21	B22	B23	
C	d	25	30	25	15	20	20	20	25	—	—	—	—	—	—	—	—	
	e	—	—	—	5	—	—	—	—	15	15	—	—	—	—	—	15	
B	e	—	—	—	—	—	5	—	—	20	—	—	15	15	—	—	—	
	f	—	—	—	—	5	—	—	—	—	—	—	10	—	—	15	—	
g	g	49	39	59	54	42	34	5	11	39	74	66	64	44	44	26	30	
	h	—	—	—	10	17	—	39	—	—	8	20	—	—	53	—	—	
i	i	—	—	—	—	—	—	10	20	48	—	—	—	5	25	—	49	
	j	10	—	—	—	—	—	—	—	—	20	—	—	—	—	—	—	
k	k	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	
	l	—	15	—	—	—	—	—	—	15	—	—	—	—	—	—	—	
m	m	—	—	—	—	—	15	—	—	—	—	—	15	—	—	—	—	
	n	10	10	10	5	5	—	10	10	—	—	—	—	—	—	—	—	
o	o	—	—	—	5	5	10	—	—	5	5	—	15	—	—	—	—	
	p	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
q	q	5	5	5	5	5	5	5	5	—	—	—	—	—	—	—	—	
	r	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	
s	s	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	—	—	—	—	—	—	—	—	
	t	—	—	—	—	—	—	—	5	5	5	5	5	5	5	5	5	
u	u	—	—	—	—	—	—	—	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	

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- a. Kind of solution A
- b. Kind of solution B
- c. Composition
- d. Haiparon 20
- e. Nipōru
- f. Zettōpōru
- g. Methyl methacrylate
- h. Butyl methacrylate
- i. 2-ethylhexyl methacrylate
- j. Isobornyl methacrylate
- k. Acrylonitrile
- l. Styrene
- m. Vinyl acetate
- n. Methacrylic acid
- o. Hydroxyethyl methacrylate
- p. Ethylene glycol dimethacrylate
- q. Cumene hydroperoxide
- r. 2,5-di-tertiary-butyl-hydroquinone
- s. Cobalt naphthenate
- t. Butylaldehyde-aniline condensate
- u. Nokuserā-8
- v. OI blue

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Next, the various solutions A and B shown in Table 6 above were selected as shown in Table 7 below, and resins and sanded spec copper plates were each adhered to each other. In the adhesion, in the case in which the solutions A and B were used without being mixed and the case in which they were used after being mixed, as in Actual Examples 20-25, the tensile shear strengths were compared. The measurements were performed under the same conditions as in Actual Examples 20-25. These results are shown in Table 7 below.

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Table 7

		a												
		26	27	28	29	30	31	32	33	34	35	36	37	38
b		A 20	A 17	A 21	A 22	A 18	A 18	A 19	A 16	A 23	A 18	A 22	A 23	A 16
c	(°C)	80.4	115.7	58.5	29.9	113.1	113.1	91.3	124.6	22.6	113.1	29.9	22.6	124.1
d		B 19	B 16	B 20	B 22	B 17	B 18	B 22	B 21	B 17	B 23	B 16	B 16	B 33
e	(°C)	80.4	122.7	69.2	41.4	101.4	90.8	41.4	61.3	101.4	29.9	122.7	122.7	23.9
f	(°C)	0.0	7.0	10.7	11.5	11.7	22.3	49.9	63.3	78.8	88.2	92.8	100.1	100.2
g		h	164	211	137	65	218	196	131	166	105	77	72	63
		i	171	229	159	89	238	216	160	181	125	126	127	120
	(kg/cm)	j	152	197	115	44	197	170	89	96	73	39	43	35
k		h	175	226	153	82	230	211	162	190	145	147	150	149
		i	182	241	160	91	243	218	175	201	154	165	167	170
	(kg/cm)	j	168	219	145	73	222	199	153	178	130	126	129	132

50 a. Actual Examples
 b. Kind of solution A
 c. Secondary transition temperature T_{gA}
 of monomer composition copolymer in
 solution A
 d. Kind of solution B
 e. Secondary transition temperature T_{gB}
 of monomer composition copolymer in
 solution B

55 f. Difference between T_{gA} and T_{gB}
 g. Tensile shear strength by non-mixed
 adhesion
 h. Average value
 i. Maximum value
 j. Minimum value
 k. Tensile shear strength by mixed adhe-
 sion

From these results, it can be seen that when solutions A and B are used without mixing, the scattering

of the adhesive strength is smaller, the smaller the difference is between the secondary transition temperatures T_{gA} and T_{gB} of the monomer composition copolymers of solutions A and B, and that when solutions A and B are mixed before use, the scatter of the adhesive strength is small regardless of the difference between T_{gA} and T_{gB} .

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(Actual Examples 39-50, Comparison Examples 14, 15)

Solutions A and B shown in Tables 1 and 2 were selected according to Table 8 below, and adhesive compositions with different ratios of the total elastomer quantity to the quantity of chlorosulfonated polyethylene in the adhesive composition, when the solutions A and B were used in equal quantities, were prepared. These adhesives were used to adhere resins to each other and sanded spec copper plates to each other; after leaving [these samples] at room temperature for 1 day, their tensile shear strengths were measured. Furthermore, these adhered bodies were left for 2 months at 120 °C, after which the temperature was returned to 20 °C and the tensile shear strengths were measured; their resistances to thermal deterioration were compared. Moreover, after letting the adhered bodies cure for 3 days at room temperature after adhesion, their impact strengths were measured. These results are shown in Table 8 below.

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Table 8

	a										b			
	39	40	41	42	43	44	45	46	47	48	49	50	14	15
c	A 2	A 1	A 2	A 3	A 4	A 8	A 5	A 5	A 9	A 3	A 3	A 3	*	-
d	(%)	30	35	30	25	20	20	12.5	12.5	15	25	25	25	30
e	(%)	0	0	0	0	0	5	0	0	15	0	0	0	0
f	B 7	B 5	B 4	B 9	B 2	B 3	B 2	B 1	B 2	B 13	B 14	B 15		
g	(%)	5	10	12.5	15	20	17.5	20	25	20	0	0	0	0
h	(%)	0	0	0	0	0	0	0	0	0	10	15	0	
$(X_{a1} + X_{b1} + X_{b2}) \times 100$		16.7	23.6	41.7	60	100	112.5	160	200	223.3	0	40	80	0
$\frac{X_{a1}}{X_a}$		210	203	200	178	165	178	143	96	87	206	77	192	238
i	j	120 c.	k	105	143	150	142	141	135	126	130	123	144	112
		(kg/cm ²)											94	130
l	j	238		231	225	220	198	215	176	137	124	240	98	210
		(kg/cm ²)											-	-
m	k	142		195	216	229	217	221	207	193	138	185	120	113
n	(kg · cm/cm ²)	14		17	16	17	17	16	14	12	9	10	5	6
													12	15
													14	14

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- a. Actual Examples
- b. Comparison Examples
- c. Kind of solution A
- 5 d. Chlorosulfonated polyethylene content
 X_a in solution A
- e. NBR content X_{a1} in solution A
- f. Kind of solution B
- 10 g. NBR content X_{b1} in solution B
- h. Content X_{b2} of other elastomer ingredient in solution B
- i. Tensile shear strength with non-mixed adhesion
- j. Initial period
- k. After 2 months at 120°C
- l. Tensile shear strength with mixed adhesion
- m. Impact strength when non-mixed adhesion was performed
- n. Impact strength when mixed adhesion was performed
- o. *: non-mixed type used.

15 From these results, it can be seen that the combinations of solutions A and B in which the ratio of the total elastomer ingredient to the quantity of chlorosulfonated polyethylene was 28.5-160 wt % had excellent adhesive strengths, resistances to thermal deterioration, and impact strengths, and that these properties were better with the mixed adhesion than with the non-mixed adhesion.

20 (Actual Examples 51-64, Comparison Examples 16-19)

First, solutions A and B were prepared as shown in Tables 9 and 10 below. The thixo[tropy] coefficients and spinnabilities of the various solutions were measured.

25 The thixo coefficients were obtained by measuring the empirical viscosity with two revolutions η_2 and the empirical viscosity with 20 revolutions η_{20} at 20°C, using a type B viscometer, and taking their ratio η_2/η_{20} . The spinnability was obtained by pulling a glass rod from a container containing a solution A or B and checking the ease with which the thread of the adhesive was cut and the spinning time, etc.; those solutions which were easy to cut are shown as O, those which were somewhat difficult to cut as Δ, and those which could be pulled to a great degree as x.

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Table 9

		A 24	A 25	A 26	A 27	A 28	A 29	A 30	A 31	A 32*	A 33*
a	b	25	25	20	15	12.5	25	8	20		
c	c	5	—	—	—	—	—	—	—		
d	e	1.5	—	—	—	—	—	—	—		
e	d	—	2.5	2.5	—	—	—	—	—		
g	g	—	—	7.5	21	25	1	20	—		
h	h	43.5	52.5	55	50	48.5	60	53	56		
i	i	5	—	5	—	—	—	—	—		
j	j	10	5	5	10	10	10	10	10		
k	k	—	5	—	—	—	—	—	—		
l	l	2	2	2	2	2	2	2	2		
m	m	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5		
n	n	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5		
o	o	5	10	50	140	200	4	250	0	—	—
p	η_z	40000	15300	28000	106000	122000	22000	95000	23000	10600	5000
	η_z / η_{10}	26000	8500	10600	18000	20000	18200	15000	21000	9700	4500
q	o	o	o	o	o	o	o	o	o	x	x
q	o	o	o	o	o	o	o	o	o	x	x

a. Composition
 b. Halparon
 c. Niporu
 d. Styrene block copolymer
 e. Kureiton
 f. Correction July 28, 1989
 g. Acrylic resin Paracold A-30
 h. Methyl methacrylate
 i. Styrene
 j. Methacrylic acid
 k. Hydroxyethyl methacrylate
 l. Ethylene glycol dimethacrylate
 m. 2,5-tertiary-butyl-hydroquinone
 n. Cumene hydroperoxide
 o. Wt % of styrene block copolymer with respect to elastomer ingredient
 p. Thixotropy
 q. Spinnability
 r. *: Other company's product used

Table 10

N.B.R	C	B24 B25 B26 B27 B28 B29 B30 B31								R.3?	R.3?
		b	b	b	b	b	b	b	b		
a	C	2.0	15	—	—	5	2.0	8	15	—	—
	C	—	—	12	—	5	—	—	—	—	—
	d	—	—	—	10	—	—	—	—	—	—
	f	1	—	—	—	—	0.5	—	—	—	—
	f	—	1.5	—	—	—	—	—	—	—	—
	h	—	—	6	14	20	—	2.4	0.5	—	—
		6.4	66.5	72	66	60	69.5	58	60	—	—
		—	—	5	7	—	—	—	—	—	—
	k	—	2	2	2	2	2	2	2	—	—
	l	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	—	—
	m	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	—	—
	n	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	—	—
	o	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	—	—
	p	5	10	50	140	200	2.5	300	3.3	—	—
	q	1/ η_{20}	23100	17600	8750	33000	65000	11000	108000	17600	108000
		1/ η_{20}	13600	4000	3500	7500	12500	8300	18000	16000	9000
		η_2 / η_{20}	1.7	1.9	2.5	4.4	5.2	1.3	6.0	1.1	1.2
	r	O	O	O	O	O	X	O	X	X	X

a. Composition
 b. Other company's product
 c. Niporu
 d. Zettoporu
 e. Styrene block copolymer
 f. Kurelton
 g. Correction July 28, 1989
 h. Acrylic resin Paracold A-30
 i. Methyl methacrylate
 j. Styrene

k. Ethylene glycol dimethacrylate
 l. 2,5-tertiary-butyl-hydroquinone
 m. Cobalt naphthenate
 n. Accelerator 808
 o. Oil red
 p. Wt % of styrene block copolymer with respect to elastomer ingredient
 q. Thixotropy
 r. Spinnability

Moreover, the spinnabilities of mixtures of the various solutions A shown in Table 9 and the solution B26 shown in Table 10, at a 1/1 weight ratio, mixed by hand for 30 seconds, and mixtures of the various solutions B shown in Table 10 and the solution A25 shown in Table 9, mixed by hand in the same way, were measured, and these results are shown in Tables 11 and 12.

In addition, using these mixtures of solutions A and B, resins were adhered to each other and sandblasted spec copper plates were adhered to each other; after curing for 1 day at room temperature, their tensile shear strengths were measured. These results are also shown in Tables 11 and 12 below.

Table I

	a								b		
	51	52	53	54	55	56	57	58	16	17	
c	A24	A25	A26	A27	A28	A29	A30	A31	A32	A33	
d	○	○	○	○	○	△	○	×	×	×	
e	(kg/cd)	210	219	200	173	161	220	97	211	215	130

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Table 12

	a								b		
	59	60	61	62	63	64	65	66	18	19	
C	B24	B25	B26	B27	B28	B29	B30	B31	B32	B33	
D	O	O	C	O	O	X	O	X	—	—	
E	(kg/cm)	208	230	219	196	165	215	112	197	215	130

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- a. Actual Examples
- b. Comparison Examples
- c. Kind of solution B

- d. Spinnability when mixed with A25
- e. Adhesive strength

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Claims

(1) A two-solution acrylic adhesive composition, consisting of a solution A, in which the following ingredients (1)-(3) are dissolved and mixed as necessary ingredients, in the proportions mentioned below, and a solution B, in which the following ingredients (4)-(6) are dissolved and mixed as necessary ingredients, in the proportions mentioned below:

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Solution A	
(1) Chlorosulfonated polyethylene	12.5-35 wt %
(2) At least one (meth)acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)acrylates with hydroxyl, glycidyl, or amino groups	50-85 wt %
(3) Organic peroxide	0.2-10 wt %

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(2) A two-solution acrylic adhesive composition in accordance with Claim (1), in which a butadiene-acrylonitrile copolymer elastomer is contained in the aforementioned solution A, and the proportions of the elastomer content in solution A (W_a) and the elastomer content in solution B (W_b) are such that $W_a/W_b = 0.5-3.0$, by weight.

(3) A two-solution acrylic adhesive composition in accordance with Claim (1) or Claim (2), in which at least one of the aforementioned solutions A or B contains at least one styrene block copolymer, selected from a group including styrene-butadiene-styrene block copolymers, styrene-isoprene-styrene block copolymers, styrene-ethylene-butylene-styrene block copolymers, styrene-ethylene-propylene-styrene block copolymers, styrene-butadiene block copolymers, styrene-isoprene block copolymers, styrene-ethylene-butylene block copolymers, and styrene-ethylene-propylene block copolymers.

(4) A two-solution acrylic adhesive composition in accordance with Claim (3), in which the aforementioned styrene block copolymer has the proportion of 5-200 wt % with respect to the elastomer ingredient contained in the solution A or B which contains this styrene block copolymer.

(5) A two-solution acrylic adhesive composition in accordance with any of Claims (1)-(4), in which the butadiene-acrylonitrile copolymer elastomer is a hydrogenated nitrile rubber.

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㉕ Two-solution acrylic adhesive composition.

㉖ A two-solution acrylic adhesive composition, consisting of a solution A, in which the following ingredients (1)-(3) are dissolved and mixed as necessary ingredients, in the proportions mentioned below, and a solution B, in which the following ingredients (4)-(6) are dissolved and mixed as necessary ingredients, in the proportions mentioned below:

Solution A: (1) 12,5-35 wt% chlorosulfonated polyethylene, (2) 50-85 wt% of at least one (meth)acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)acrylates with hydroxyl, glycidyl, or amino groups and (3) 0,2-10 wt% of a organic peroxide;

Solution B: (4) 10-25 wt% butadiene-acrylonitrile copolymer elastomer, (5) 40-90 wt% of at least one (meth)acrylate selected from a group consisting of (meth)acrylic acid, (meth)acrylate, di(meth)acrylate, and (meth)acrylates with hydroxyl, glycidyl, or amino groups, and (6) 1-20 wt% of a curing accelerator consisting of an amine-aldehyde condensate. This adhesive composition has excellent resistance to thermal deterioration and excellent workability.

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European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

EP 89 12 4145

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.5)						
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim							
Y,D	FR-A-2 193 863 (E.I. DU PONT DE NEMOURS AND CO.) * Claims 1-3,5; page 1, lines 37-38; page 2, lines 1-26 * & JP-A-49 132 119 ---	1	C 09 J 4/06						
Y	US-A-4 200 480 (L.E. WOLINSKI et al.) * Claims 1,2; page 4, lines 42-53 * ---	1							
A	EP-A-0 044 166 (LOCTITE CORP.) * Claim 1 * ---	3							
A	US-A-4 548 992 (H. DOI et al.) * Page 4, lines 17-25; claim 1 * & JP-A-58 096 666 -----	5							
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)						
			C 09 J						
<p>The present search report has been drawn up for all claims</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">Place of search</td> <td style="width: 33%;">Date of completion of the search</td> <td style="width: 34%;">Examiner</td> </tr> <tr> <td>THE HAGUE</td> <td>18-10-1990</td> <td>ANDRIOLLO G.R.</td> </tr> </table>				Place of search	Date of completion of the search	Examiner	THE HAGUE	18-10-1990	ANDRIOLLO G.R.
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